

# **Extraction of sulfur compounds from liquid** fuels with the addition of oxidizing agent

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### ABSTRACT:

Hydrodesulfurization (HDS), a widely employed method in industries for the desulfurization of fuel oils, such as gasoline and diesel fuel, is faced with the challenge of producing lower-sulfur or sulfur-free fuel oils, which are required by more and more countries. However, HDS is not very effective for the removal of thiophenic sulfur compounds, unless operated under harsh conditions, such as high temperature, high pressure, and requirement of a noble catalyst and hydrogen. Extractive desulfurization (EDS) and oxidative desulfurization (ODS) of fuel oils using ionic liquids (ILs) has been intensively studied in recent years by our team and has a good future as an alternative or complementary method to HDS.

In this study, we present experimental data of liquid-liquid phase equilibrium (LLE) for the ternary systems [BMMOR][TCM] or [HMMOR][TCM] (1) + thiophene, or benzothiophene (2) + heptane (3)) at temperature and that the substitution of the substitution of the substitution of the proper of the substitution of the experimental equilibrium data, were calculated and used to determine the efficiency of these ionic liquid as a solvent for the extraction of sulfur compounds from model fuels. The experimental data were correlated using the NRTL equation [1], and the binary interaction parameters have been reported.

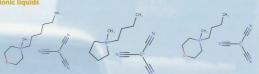
that were contained.

In the second part of our experiment, the oxidative desulfurization of model fuels has been studied using thrityanomethanide-based ionic liquid. Model liquid fuel was prepared by dissolving aromatic sulfur compounds in alkane. Oxidation in this process was achieved by adding hydrogen peroxide and acetic acid to the mixture. Different parameters such as oil to IL, or DES ratio, oxidant to sulfur ratio, temperature

were optimized.

Based on our research, we can conclude that EDS and ODS using ILs are a potentially preferable methods to remove thiophenic S compounds compared to traditional HDS technology.

## **MATERIALS**









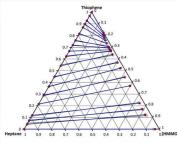


Fig. 1. Experimental tie-lines (•, black lines) Fig. 1. Experimental tue-lines (•, black lines) for the LLE of the ternary system  $\{|HMMOR||TCM|\ (1) + \text{thiophene}\ (2) + \text{heptane}\ (3)\}$  at T=308.15 K and p=0.1 MPa. The corresponding tie-lines orrelated by means of the NRTL equation  $(\circ, \text{blue lines})$ .

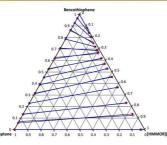


Fig. 2. Experimental tie-lines (•, black lines) for the LLE of the terrors Fig. 2. Experimental te-lines (•, black lines) for the LLE of the ternary system [HMMOR][TCM] (1) + benzothiophene (2) + heptane (3)) at T = 308.15 K and p = 0.1 MPa. The corresponding tie-lines correlated by means of the NRTL equation (o, blue lines).

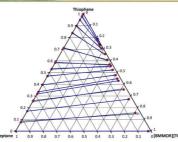


Fig. 3. Experimental tie-lines (•, black lines) for the LLE of the ternary system Fig. 3. Experimental tie-lines (•, black lines) for the LLE of the ternary system [BMMOR][TCM] (1) + thiophene (2) + heptane (3)) at T = 308.15 K and p = 0.1 MPa. The corresponding tie-lines correlated by means of the NRTL equation (⋄, blue lines).

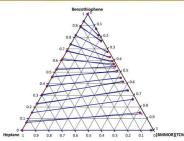


Fig. 4. Experimental tie-lines (•, black lines) for the LLE of the terrors Fig. 4. Experimental tie-lines  $(\bullet, black lines)$  for the LLE of the ternary system [BMMOR][TCM] (1) + benzothiophene (2) + heptane (3)] at T=308.15 K and p=0.1 MPa. The corresponding tie-lines correlated by means of the NRTL equation  $(\circ, blue lines)$ .

**Table 1.** Binary interaction parameters and root mean square deviation  $(\sigma_x)$  for the NRTL equation for ternary systems {[BMMOR][TCM] or [HMMOR][TCM] (1) + thiophene or benzothiophene (2) + heptane (3)} at T=308.15 K, p = 0.1 MPa. Parameter  $\alpha_{ij} = \alpha_{ji} = 0.2$ 

Components i-j	NRTL parameters		
	g <sub>ij</sub> -g <sub>jj</sub> (J mol⁻¹)	8 <sub>ji</sub> *8 <sub>ii</sub> (J mol⁻¹)	RMSE $\sigma_{x}$
[BMMOR][TCM	I] (1) + thiophen	e (2) + heptane (3)	
1-2	1930.4	58458	0.006
1-3	5659.7	15880	
2-3	3023.3	1378.3	
[BMMOR][TCM	[1] (1) + benzothic	ophene (2) + hepta	ne (3)
1-2	4703.9	68148	0.008
1-3	7127.3	15240	
2-3	756.20	5067.7	
[HMMOR][TC	M] (1) + thiophen	e (2) + heptane (3)	)
1-2	-861.03	60820	0.005
1-3	4123.0	15883	
2-3	5056.2	-1327.2	
[HMMOR][TC	vI] (1) + benzothic	ophene (2) + hepta	ne (3)
1-2	1581.0	66983	0.006
1-3	5262.3	14960	
2-3	3448.0	600.52	

$$S = \frac{x_2^{II} \cdot x_3^I}{x_2^I \cdot x_3^{II}}$$

$$\beta = \frac{x_2^{II}}{x_2^{I}}$$

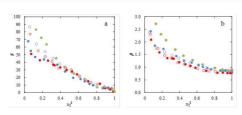
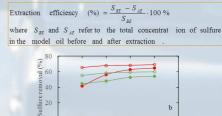
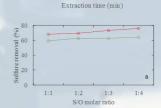


Fig. 5. Plots of the selectivity (a) and solute distribution ratio (b) as a function Fig. 5. Plots of the selectivity (a) and solute distribution ratio (b) as a function of the mole fraction of solute in the hydrocarbon – rich phase for the ternary systems:

(a) {[BMMOR][TCM] (1) + benzothiophene (2) + heptane (3)};
(b) {[BMMOR][TCM] (1) + bincomplete (2) + heptane (3)};
(c) {[HMMOR][TCM] (1) + benzothiophene (2) + heptane (3)}; (  $\bullet$  ) {[BMPYR][TCM] (1) + thiophene (2) + heptane (3)} at  $T = 298.15 \,\mathrm{K}$  [2]

The oxidative-extractive desulfurization of model fuels has been studied using tricyanomethanide-based ionic liquid. Model liquid fuel was prepared by dissolving benzothiophene in octane (500 ppm of sulfur). Oxidation in this process was achieved by adding hydrogen peroxide and acetic acid to the mixture.





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Fig. 6. The effect of extraction time (a) and the amount of oxidant (b) on sulfur removal. As extractant used: [BMMOR][TCM]:

(a) at T = 308.2 K, (b) at T = 318.2 K; [BMPYR][TCM]: (a) at T = 308.2 K, (b) at T = 318.2 K;



M. Prausnitz, R. N. Lichtenthaler, E. Gomes de Azevedo, Molecular Thermodynamics of Fluid Equilibria, Third Edition, (1999) Prentice Hall International Series in the Physical and Chemical

[2] U. Domańska, E. V. Lukoshko, M. Królikowski, J. Chem. Thermodyn. 61 (2013) 126–131.